

Pavement Number - PN -

Acknowledgements

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1

Pavement Number (PN) Design

Structural Number on Steroids

- Robust and easy to use
- Develop clear, strong links to field testing (material classification) and specifications
- First version 2008, update 2020
- Data Sets
 - 69 field sites
 - SATCC and TRH4 Catalogues
 - Construction, maintenance & performance information



2

Pavement Number (PN)

- Structural Number
 - Modified with **rules of thumb**
- Relies on “accurate” **DEMAC Material Class** input
- **Calibrated & validated**
 - Field data
 - Catalogues of design
 - Experience

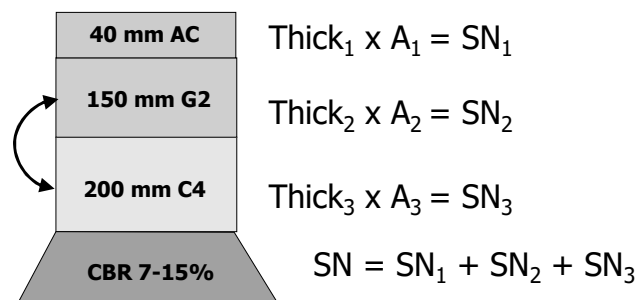
NEW



3

Disadvantages of SN Approach

- Non-uniqueness of the index
 - Switching base and subbase give same SN
- Insensitivity to placement of weak layers



These limitations are overcome by incorporating design *rules of thumb* that make the SN more “intelligent”.

4

Rules of Thumb: General

- Structural capacity is a function of:
 - The combined **long-term load spreading** of all pavement layers
 - Relative **quality of subgrade**
- Subgrade quality is the point of departure for design
- The type and quality of the **base layer** is critical

Says Who?

- *Established knowledge in guidelines and textbooks*
- *Trends in well established design catalogues (TRH4)*
- *Trends in LTPP and HVS section performance*



5

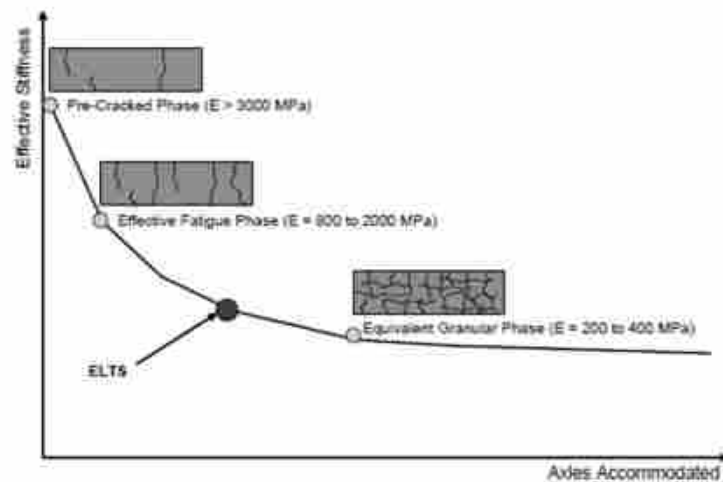
Rules of Thumb: Layers

- Effective Long Term Stiffness (ELTS)
- Modular Ratio
- Maximum Allowable Stiffness
 - *Predetermined based on Material Class*
- Base Confidence Factor



6

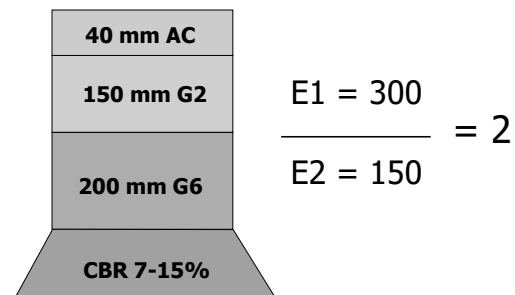
Effective Long Term Stiffness (ELTS)



7

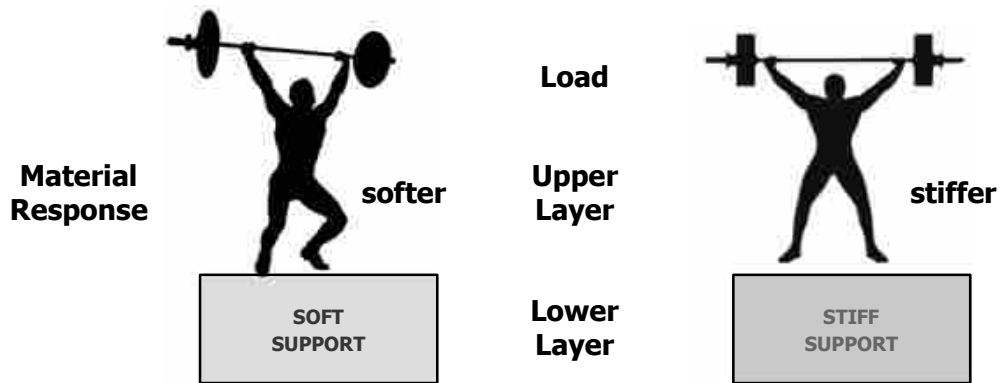
Modular Ratio

- The stiffness of one layer as a ratio of the layer underneath



8

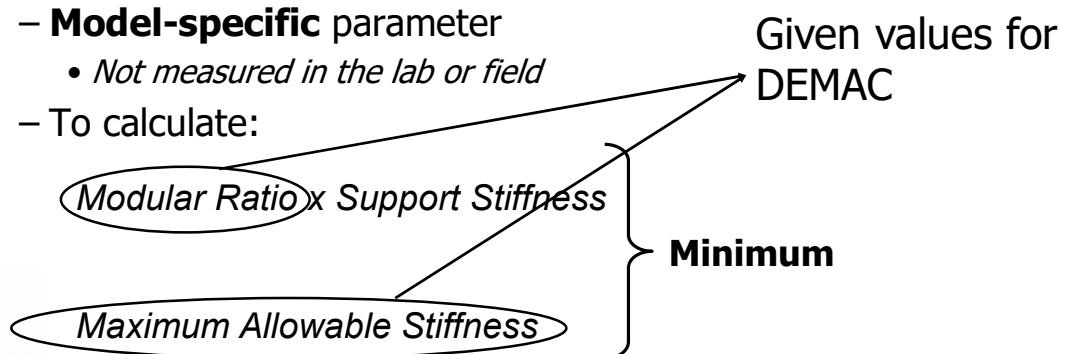
Pavement Balance



9

Effective Long Term Stiffness (ELTS)

- Represents the **average stiffness** of the material over the design life
- Depends on the **material type/quality**
- **Model-specific** parameter
 - *Not measured in the lab or field*
- To calculate:



10

Quality of Base Material

- Base Confidence Factor (BCF)
 - *Suitability of material to serve as a base layer*
- Ensures poor designs are disqualified



11

DEMAC Material Class	Thickness Limits	Modular Ratio	Max Allow. Stiffness	Base Confidence
Asphalt surfacing	20 - 100	4	2000	1
Asphalt base	20 - 200	4	1500	1
Seals	10	2	1000	N/A
BSM1	100 - 300	3	700	1
BSM2		2	600	0.7
G1	100 - 150	3	600	1
G2	100 - 200	2	450	0.8
G3		1.8	400	0.7
G4	100 - 300	1.8	375	0.2
G5		1.8	350	0.1
G6		1.8	250	-2
G7		1.7	140	-2.5
G8	100 - 350	1.6	100	-3.0
G9		1.4	90	-4.0
G10		1.2	70	-5.0
C3	100 - 350	4	500	0.6
C4		3	400	0.4
EG4	100 - 350	2	400	0.2
EG5		1.8	300	0.2



12

Climate Adjustment (Thorntwaite/Weinert)



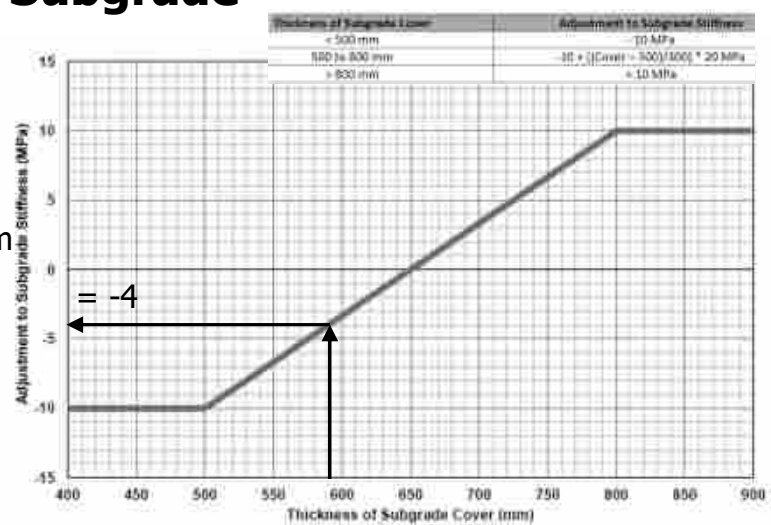
Climate	Adjustment Factor
Wet	0.6
Moderate	0.9
Dry	1.0

13

Quantifying the Subgrade

DEMAC Mat class	Thick
Seal	10
BSM2	200
C4	200
G6	180
G7	N/A

= 590 mm

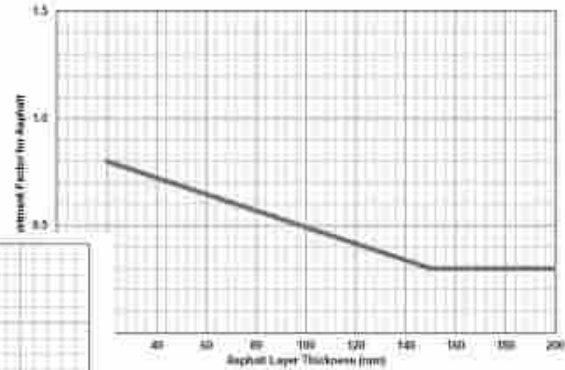
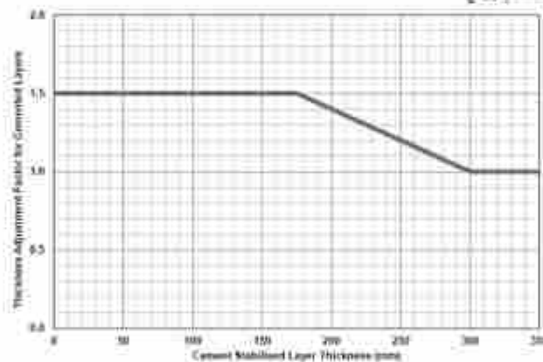


14

Thickness Adjustment Factors

– Stabilised layers

- *Asphalt surfacings and bases*
- *BSMs*
- *Cemented layers*



15

Five Layer Limit

- Pavement must have 5 layers
- Surfacing must be modelled separately
- If have got 4 layers or less
 - Add selected layer(s) 150 mm thick of same material class as subgrade
- If have more than 5 layers
 - Start with combining below subbase
 - Material class should be that of the thicker layer
 - If layers same thickness then use lower material class
 - If combine with subgrade, then assign material class of upper layer to new subgrade
 - Thickness limits must not be exceeded



16



17



18



19



20



21



22

How Does the PN Work?

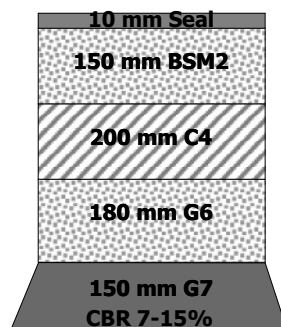
1. Determine **subgrade stiffness** based on DEMAC class
2. Adjust subgrade stiffness for **climate** and **cover depth**
3. For each layer, determine the **Modular Ratio** and **Maximum Allowed Stiffness** based on material class
4. Work up from the subgrade and determine the **ELTS** of each layer
5. Adjust base stiffness using **BCF**
6. For **stabilised materials**, adjust ELTS based on thickness
7. Multiply thickness and ELTS for each layer and sum to obtain **PN**



23

Example, Moderate Region

1. DEMAC Material Classes



2. Determine subgrade stiffness
3. Adjust for climate
4. Adjust for cover

5. Assign modular ratio's and max stiffness

MR = 2, $E_{Max} = 1000$
MR = 2.5, $E_{Max} = 600$
MR = 3, $E_{Max} = 400$
MR = 1.8, $E_{Max} = 250$
118 MPa

6. Calculate Layer ELTS Values

ELTS = 1000
ELTS = 600, BCF = 0.7 Thickness Adj = 1.0
ELTS = 400 Thickness Adj = 1.4
ELTS = min(212, 250) ELTS = 212
118 MPa

6. $ELTS = \min(E_{support} * MR, E_{max})$
7. Layer PN = thickness * ELTS * factors
8. $PN = \sum \text{layer PN}$



24

PN 2009 - Issues

- 20 actual pavement structures, heavy reliance on TRH4 catalogue
- Over contribution of asphalt
- Under contribution of cemented materials
- Asphalt surfacing
 - Limited to < 50 mm
- No asphalt bases
- Increase in PN, no increase in life
- Limited to 30 MESA



25

~~PN 2009~~ 2020

- ~~20~~⁶⁹ actual pavement structures, ~~heavy reliance on TRH4 catalogue~~ 9 different combinations of pavement structures, plus asphalt and seal surfacings
- Over contribution of asphalt ✓
- Under contribution of cemented materials ✓
- Asphalt surfacing ✓
 - Limited to < 50 mm 20 – 100 mm
- No asphalt bases ✓ 20 – 200 mm
- Increase in ~~PN~~, no increase in life ✓ New Frontier Curve
- Limited to ~~30~~ MESA ✓ 40 MESA



26

PN 2020 – What Else is New?

- Thickness adjustment factor for stabilized layers

- Asphalt
- Cemented
- BSMs
- Effect of empirical method

- Materials

- Asphalt bases
- EG 4 & 5

- Seals are 10 mm thick

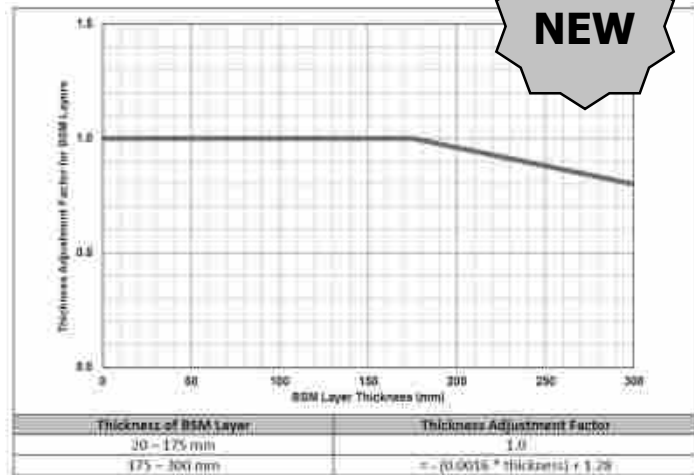


Figure C.6 Thickness Adjustment Factor for BSM Layers

27

PN Example

Subgrade class	G7
Initial stiffness	
Climate	Moderate
Climate adj	
Cover depth	
Cover adj.	
SG ELTS	

Mat class	Thick	T check	MR	Max E	ELTS	Thick adj	BCF	Layer PN
Seal	10							
BSM2	200							
C4	200							
G6	180							
G7	N/A							



28

PN Example

Subgrade class	G7
Initial stiffness	140
Climate	Moderate
Climate adj	0.9
Cover depth	
Cover adj.	-4
SG ELTS	

Design equivalent material class	Stiffness value (MPa)
G6 or better	250
G7	140
G8	100
G9	90
G10	70

Mat class	Thick	T check	MR	Max E	ELTS	Thick adj	BCF	Layer PN
Seal	10	10	2	1000			N/A	
BSM2	200	✓	2.5	600		0.96	0.7	
C4	200	✓	3	400		1.40	N/A	
G6	180	✓	1.8	250			N/A	
G7	N/A		N/A	N/A			N/A	



29

PN Example

Subgrade class	G7
Initial stiffness	140
Climate	Moderate
Climate adj	0.9
Cover depth	
Cover adj.	-4
SG ELTS	

Climate / Weinert N value	Adjustment factor
Wet (N < 2)	0.6
Moderate (N = 2 to 5)	0.9
Dry (N > 5)	1.0

Mat class	Thick	T check	MR	Max E	ELTS	Thick adj	BCF	Layer PN
Seal	10	10	2	1000			N/A	
BSM2	200	✓	2.5	600		0.96	0.7	
C4	200	✓	3	400		1.40	N/A	
G6	180	✓	1.8	250			N/A	
G7	N/A		N/A	N/A			N/A	



30

PN Example

Subgrade class	G7
Initial stiffness	140
Climate	Moderate
Climate adj	0.9
Cover depth	
Cover adj.	-4
SG ELTS	

DEMC	BSM1	BSM2
Modular Ratio	3.0	2.5
Max Allowed Stiffness	700	600
BCF	1.0	0.7
Thickness limit	100 to 300 mm	100 to 300 mm

Mat class	Thick	T check	MR	Max E	ELTS	Thick adj	BCF	Layer PN
Seal	10	10	2	1000			N/A	
BSM2	200	✓	2.5	600		0.96	0.7	
C4	200	✓	3	400		1.40	N/A	
G6	180	✓	1.8	250			N/A	
G7	N/A		N/A	N/A			N/A	

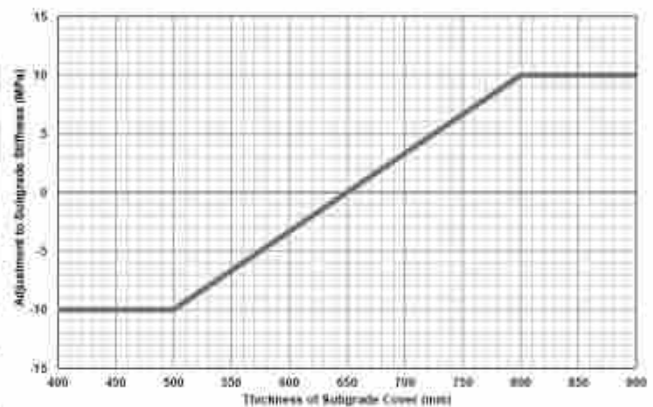


31

PN Example

Subgrade class	G7
Initial stiffness	140
Climate	Moderate
Climate adj	0.9
Cover depth	590
Cover adj.	-4
SG ELTS	

Mat class	Thick	T check	MR	Max E	ELTS	Thick adj	BCF	Layer PN
Seal	10	10	2	1000			N/A	
BSM2	200	✓	2.5	600		0.96	0.7	
C4	200	✓	3	400		1.40	N/A	
G6	180	✓	1.8	250			N/A	
G7	N/A		N/A	N/A			N/A	



32

PN Example

Subgrade class	G7
Initial stiffness	140
Climate	Moderate
Climate adj	0.9
Cover depth	590
Cover adj.	-4
SG ELTS	122

$$140 * 0.9 - 4 = 122$$

Mat class	Thick	T check	MR	Max E	ELTS	Thick adj	BCF	Layer PN
Seal	10	10	2	1000			N/A	
BSM2	200	✓	2.5	600		0.96	0.7	
C4	200	✓	3	400		1.40	N/A	
G6	180	✓	1.8	250			N/A	
G7	N/A		N/A	N/A			N/A	



33

PN Example

Subgrade class	G7
Initial stiffness	140
Climate	Moderate
Climate adj	0.9
Cover depth	590
Cover adj.	-4
SG ELTS	122

Mat class	Thick	T check	MR	Max E	ELTS	Thick adj	BCF	Layer PN
Seal	10	10	2	1000			N/A	
BSM2	200	✓	2.5	600		0.96	0.7	
C4	200	✓	3	400		1.40	N/A	
G6	180	✓	1.8	250			N/A	
G7	N/A		N/A	N/A	122		N/A	



34

PN Example

Subgrade class	G7
Initial stiffness	140
Climate	Moderate
Climate adj	0.9
Cover depth	590
Cover adj.	-4
SG ELTS	122

Mat class	Thick	T check	MR	Max E	ELTS	Thick adj	BCF	Layer PN
Seal	10	10	2	1000			N/A	
BSM2	200	✓	2.5	600		0.96	0.7	
C4	200	✓	3	400		1.40	N/A	
G6	180	✓	1.8	250	220		N/A	
G7	N/A		N/A	N/A	122		N/A	

$122 * 1.8 = 220$
 $220 < 250$
 max, 220



35

PN Example

Subgrade class	G7
Initial stiffness	140
Climate	Moderate
Climate adj	0.9
Cover depth	590
Cover adj.	-4
SG ELTS	122

Mat class	Thick	T check	MR	Max E	ELTS	Thick adj	BCF	Layer PN
Seal	10	10	2	1000	1000		N/A	
BSM2	200	✓	2.5	600	600	0.96	0.7	
C4	200	✓	3	400	400	1.40	N/A	
G6	180	✓	1.8	250	220		N/A	
G7	N/A		N/A	N/A	122		N/A	



36

PN Example

Subgrade class	G7
Initial stiffness	140
Climate	Moderate
Climate adj	0.9
Cover depth	590
Cover adj.	-4
SG ELTS	122

Calculation of layer PN

$$(600 * 200) / 10000 * 0.96 * 0.7 = 8.1$$

Mat class	Thick	T check	MR	Max E	ELTS	Thick adj	BCF	Layer PN
Seal	10	10	2	1000	1000		N/A	
BSM2	200	✓	2.5	600	600	0.96	0.7	8.1
C4	200	✓	3	400	400	1.40	N/A	
G6	180	✓	1.8	250	220		N/A	
G7	N/A		N/A	N/A	122		N/A	



37

PN Example

Subgrade class	G7
Initial stiffness	140
Climate	Moderate
Climate adj	0.9
Cover depth	590
Cover adj.	-4
SG ELTS	122

Mat class	Thick	T check	MR	Max E	ELTS	Thick adj	BCF	Layer PN
Seal	10	10	2	1000	1000		N/A	1.0
BSM2	200	✓	2.5	600	600	0.96	0.7	8.1
C4	200	✓	3	400	400	1.40	N/A	11.2
G6	180	✓	1.8	250	220		N/A	4.0
G7	N/A		N/A	N/A	122		N/A	Σ 24.2



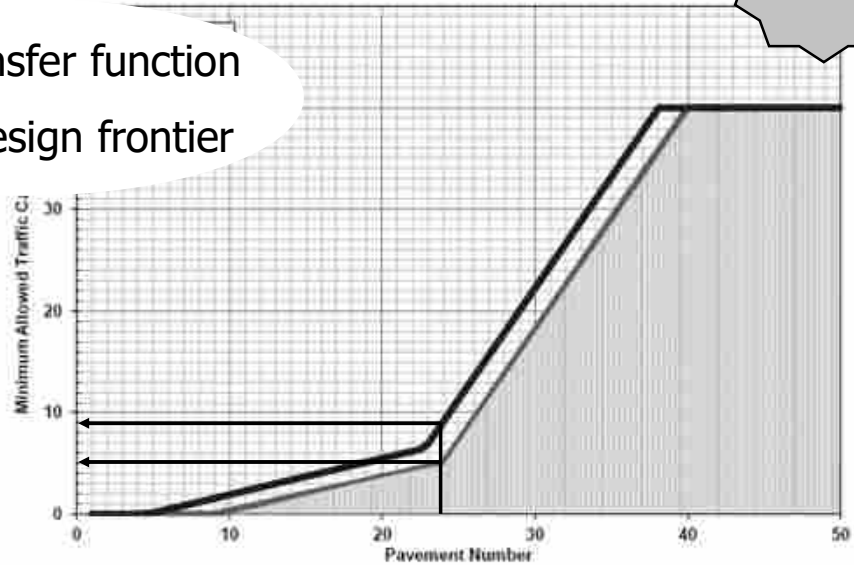
38

Design Criteria

NEW

Not a transfer function

Rather, design frontier



39

PN example

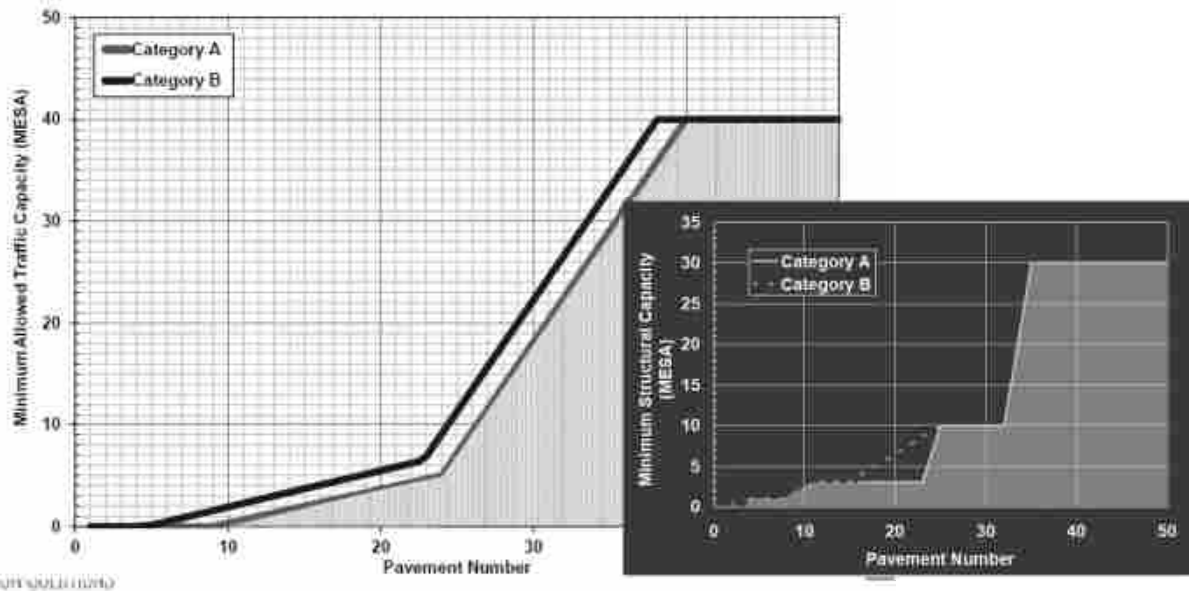
Subgrade class	G7
Initial stiffness	140
Climate	Moderate
Climate adj	0.9
Cover depth	590
Cover adj.	-4
SG ELTS	122

Cat A	5.5
Cat B	9.6

Mat class	Thick	T check	MR	Max E	ELTS	Thick adj	BCF	Layer PN
Seal	10	10	2	1000	1000		N/A	1.0
BSM2	200	✓	2.5	600	600	0.96	0.7	8.1
C4	200	✓	3	400	400	1.40	N/A	11.2
G6	180	✓	1.8	250	220		N/A	4.0
G7	N/A		N/A	N/A	122		N/A	Σ 24.2

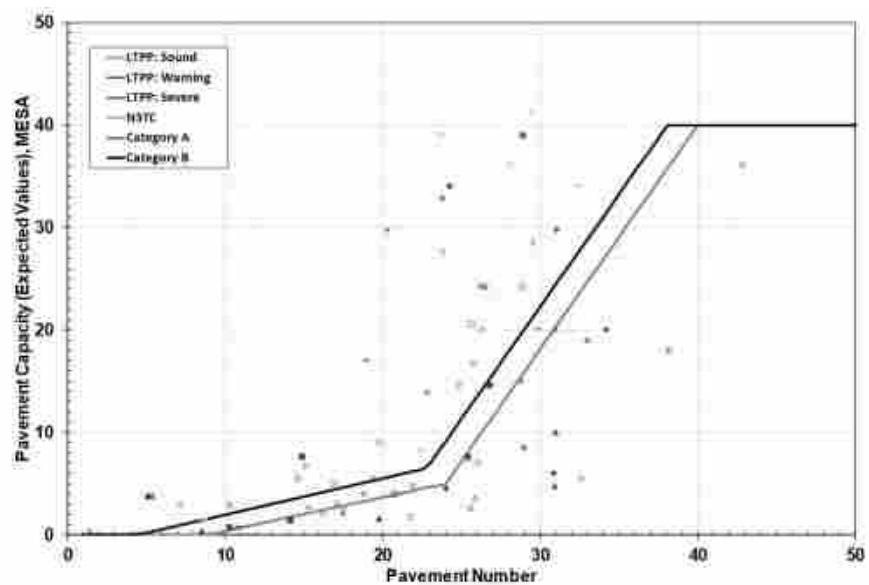
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Design Criteria



41

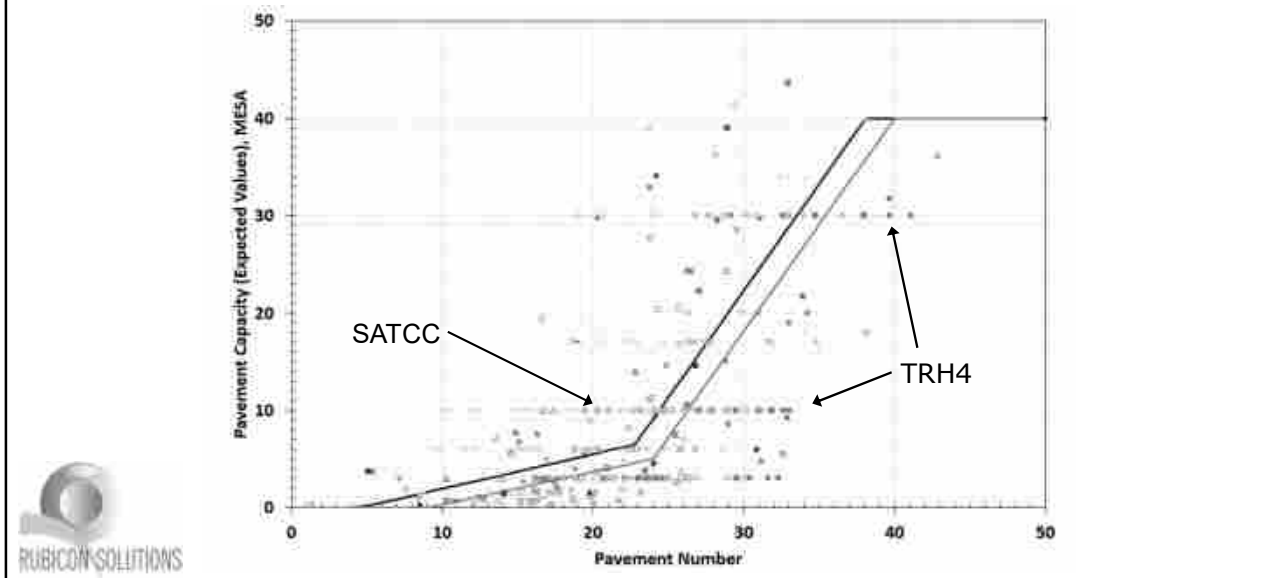
Calibration



42

PN - FRONTIER CURVE UPDATE

Calibration



43

Remarks

- Simple method, easy to understand and use
- Valid for most SA materials
- Robust, and cannot be easily manipulated
- Utilizes well known rules of thumb
- Results in balanced pavements
- Well and explicitly validated with TRH4, LTPP and HVS datasets
- Requires DEMAC Material Class as design inputs
- System rigidity may limit application



44

Hulle moet regtig die goed bietjie moeiliker
maak !

